

Transient regime to fluidized chimney within a granular bed by means of a 2D DEM/LBM modeling

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ABSTRACT

A fluidized state within a granular bed is reached when the upward force exerted by the flow can balance the buoyant weight of the particles. This may also occur in a localized manner when the fluidization is induced by a small fluid injection at the bottom of a grain pack. Many industrial processes rely on such liquid-solid fluidized beds, often showing cases of localized fluidization (spouted beds). In the context of dike safety, a seepage flow through the foundation of an embankment is susceptible to generate such a local fluidization, called “sandboil”, and possibly initiate a piping process by backward erosion, one of the four general processes reported for internal erosion [1]. Several previous studies have addressed specifically this question and analysed the formation of a vertical chimney of fluidized soil, either through experiments [2, 3] or numerical simulations coupling Discrete Element Method (DEM) and Lattice Boltzmann Method (LBM) [4]. However, most efforts have been concentrated on the steady fluidized chimney while little is yet known about the transitory development of fluidization before reaching this final chimney [3].

In the present study, a systematic analysis of the transient regime to fluidized chimney is carried out by means of numerical simulations based on a 2D DEM/LBM modelling. The results reveal that a critical fluid velocity U_c can be defined fairly precisely from the divergence of the duration of the transient regime T_0 . Then the critical velocity U_c was evaluated in a systematical and consistent way for ten different parameter sets by changing either grain properties (density, diameter) or fluid properties (viscosity, density), or reducing the acceleration of gravity by a factor of ten. A scaling law can be proposed for U_c as a function of grain diameter, fluid viscosity and reduced gravity. Introducing the relevant dimensionless numbers of the problem, namely Reynolds number Re and Archimedes number Ar , this law is simply equivalent to $Re_c \propto Ar^{3/4}$ where Re_c incorporates the critical velocity U_c . Moreover, by defining an expansion rate $V_0 = T_0/H_0$, and a related Reynolds number Re_0 , it is finally demonstrated that not only the critical velocity but also the whole transient kinetics can be accounted for by a general relation that reads: $Re_0/Re_c \propto (Re/Re_c - 1)^{3/5}$.

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