

Gait and Posture Responses to backpack load

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Abstract

The role played by the trunk in gait is relatively unexplored in the literature. Considering that the upper body makes up two third of the body weight and to look at its role as being purely passive is a puzzling hypothesis. This paper investigates the postural strategies to adapt to walking with a backpack load. The aim of the current work is to explore the possibility of using simple models to study the role played by the upper body during specific tasks (in the present reported work walking up an inclined surface with a backpack).

The simple model used in this paper depict the body as being made up of a hip of mass m_H at a position (x_H, y_H) at time t , and a trunk of mass m_T at a position (x_T, y_T) . The trunk is modulated via a torque τ between the stance leg and the trunk. It is assumed that the legs are massless. The fluctuations of the leg length $q(t)$ due to flexion of the lower joints, namely, hip, knee and ankle are incorporated in a single telescopic axial actuator that carries a compressive force $F(t)$. The leg has a maximum allowable leg extension, such that $\sqrt{x_H^2 + y_H^2} = R + q(t)$, where R is the nominal length of the leg. It is assumed that during the stance phase, the foot in contact with the ground does not slip, and at most one foot can be in contact with the ground at any given time, and that there is no flight phase. The left and right legs have identical force and length profiles.

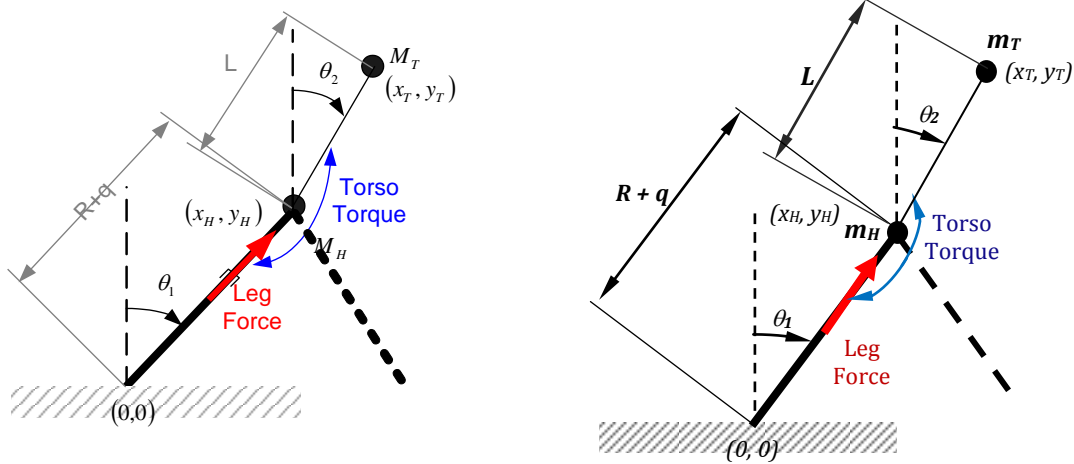


Figure 1: A Schematic of the model used

A gait is characterized by the position and velocity of the hip mass and trunk mass, by the step period and by $F(t)$ and the torque $\tau(t)$ and the maximum allowed leg extension. The equations of motion were derive using Lagrange formulation and yielded the following dynamic equations:

$$(R + q)^2(m_H + m_T)\ddot{\theta}_1 + (R + q)Lm_T \cos(\theta_1 - \theta_2) \ddot{\theta}_2 + 2(m_H + m_T)(R + q)\dot{q}\dot{\theta}_1 + (R + q)Lm_T \sin(\theta_1 - \theta_2) \dot{\theta}_2^2 - (R + q)g(m_H + m_T) \sin(\theta_1) = \tau \quad (1.a)$$

$$(R + q)Lm_T \cos(\theta_1 - \theta_2) \ddot{\theta}_1 + L^2 m_T \ddot{\theta}_2 + Lm_T \sin(\theta_1 - \theta_2) \ddot{q} - Lm_T \sin(\theta_1 - \theta_2) (R + q) \dot{\theta}_1^2 + 2Lm_T \cos(\theta_1 - \theta_2) \dot{q} \dot{\theta}_1 - Lm_T g \sin(\theta_2) = -\tau \quad (1.b)$$

$$Lm_T \cos(\theta_1 - \theta_2) \dot{\theta}_2^2 (m_H + m_T) g \cos(\theta_1) = F \quad Lm_T \sin(\theta_1 - \theta_2) \ddot{\theta}_2 + (m_H + m_T) \ddot{q} - (m_H + m_T) (R + q) \dot{\theta}_1^2 - \quad (1.c)$$

Where, θ_1, θ_2 are as defined in Fig. 1, L is distance from hip to the center of mass of the torso, and g is the gravitational constant. To reduce the number of parameters scaling was used. Scaling shows its effectiveness in gait analysis and meant that the equations are not anymore belonging to any dimension thus the person could be treated as an ensemble of ratios.

After scaling the equation of the model using, $M = m_T + m_H$; R, g and $t_c = \sqrt{R/g}$, the only two free parameters remaining are m_T/M and L/R . The optimizer will seek solutions as three parameters are varied, namely, normalized speed V , and normalized step length D and m_T/M . The remaining parameter, namely L/R will be fixed.

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