

## NON-CONFORMING SPECTRAL APPROXIMATIONS FOR THE ELASTIC WAVE EQUATION IN HETEROGENEOUS MEDIA

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**Abstract.** *Non-conforming techniques as the Mortar spectral Element Method (MSEM) or the Discontinuous Galerkin Spectral Element Method (DGSEM) are variational approaches to discretize partial differential equations, that rely on a spectral finite element approximation of a non-overlapping subdomain partition of the computational domain. In this contribution we compare and analyse MSEM and DGSEM, giving more details on the algorithmic aspects of the two non-conforming approaches, and we address their applicability and flexibility to handle seismic wave propagation problems. The numerical strategies are implemented in the spectral elements based code GeoELSE [14].*

## 1 INTRODUCTION

During the last three decades seismology is undergoing a major transformation at both the research and the application level. In modern seismology the classical scientific approach based on laboratory experiments has been replaced by computer simulations. Indeed, the rapid development of efficient numerical methods, gives the chance to simulate, with high resolution the complete seismic waveform field in highly heterogeneous earth media with complex geometries and up to relatively large frequencies (about 3 Hz).

The recent developments on computational seismology have been based on high-order numerical modelling of wave propagation (see, for example, [5, 12, 13, 15, 16, 17]). The reasons for using spectral element based approximations are the following. Firstly the flexibility in handling complex geometries, retaining the spatial exponential convergence for locally smooth solutions. Secondly, spectral element methods are based on the weak formulation of the elastodynamic equations involving only first-order spatial derivatives. Finally spectral element methods retain a high level parallel structure, and are therefore well suited for parallel computers.

In this paper we consider two different non-conforming high-order techniques, namely the Mortar Spectral Element Method (MSEM) and the Discontinuous Galerkin Spectral Element Method (DGSEM) to simulate seismic wave propagation in heterogeneous media. In contrast to standard conforming discretizations, as Spectral Element Method (SEM), these techniques have the further advantages that they can accommodate discontinuities, not only in the parameters, but also in the wave-field, they are energy conservative and well suited for parallel implementation. In our contribution we compare their performances when effectively applied to real problems. The paper is organized as follows. In Section 2 we recall the model problem under investigation. In Section 3 the non-conforming formulations are summarized. In Sections 4 we introduce the corresponding algebraic formulations and next, in Section 5 we describe how two efficiently implement them in a numerical code. In order to show an effective application of the methods previously described, in Section 6 a complex soil-structure interaction is studied using the MSEM and the DGSEM discretizations. Finally, in Section 7, we draw some conclusions.

## 2 FORMULATION OF PROBLEM

Fixing the temporal interval  $(0, T]$ , with  $T > 0$ , the equilibrium equations for an elastic medium, occupying a finite region  $\Omega \subset \mathbb{R}^d$ ,  $d = 2, 3$ , subjected to an external force  $\mathbf{f}$  read:

$$\rho \partial_{tt} \mathbf{u} - \nabla \cdot \underline{\sigma}(\mathbf{u}) = \mathbf{f} + \mathbf{f}^{visc}(\dot{\mathbf{u}}, \mathbf{u}), \quad (1)$$

where  $\mathbf{u}$  is the displacement of the body,  $\underline{\sigma}$  the stress tensor,  $t$  the time and  $\rho$  the density of the material. Since we are dealing with viscoelastic materials, we introduce in model (1) a structural damping in the form of volumetric forces  $\mathbf{f}^{visc}(\dot{\mathbf{u}}, \mathbf{u}) = -2\rho\zeta\dot{\mathbf{u}} - \rho\zeta^2\mathbf{u}$ , where  $\zeta$  is a spatially variable (i.e., piecewise constant) suitable decay factor with dimension of inverse of the time [8]. It is worth remarking that the introduction of  $\mathbf{f}^{visc}$  in (1) results in a frequency proportional quality factor, i.e. a non dispersive wave propagation (for further details see [18]). We denote by  $\Gamma = \Gamma_D \cup \Gamma_N \cup \Gamma_{NR}$  the boundary of the physical domain  $\Omega$  and without loss of generality on the boundary  $\Gamma$  we make the following assumptions (cf [22]):

- on  $\Gamma_D$  the body is rigidly fixed in the space,
- on  $\Gamma_N$  we prescribe surface tractions ( $\underline{\sigma}(\mathbf{u}) \cdot \mathbf{n} = \mathbf{t}$ ),
- on  $\Gamma_{NR}$  non-reflecting boundary conditions are imposed: cf. [27], for example.

Hereafter, an underlying bar denotes matrix or tensor quantities, while vectors are typed in bold. Moreover, we adopt the standard notation  $(\cdot, \cdot)_\Omega$  to denote the  $L^2$ -inner product for scalar, vectorial and tensorial functions defined in  $\Omega$ . To ease of presentation we describe the numerical methods in the case of null viscoelastic forces, i.e.  $\mathbf{f}^{visc}(\dot{\mathbf{u}}, \mathbf{u}) = 0$  (see Section 4.1 below for the general case).

Defining  $V = \{\mathbf{v} \in [H^1(\Omega)]^d : \mathbf{v} = \mathbf{0} \text{ on } \Gamma_D\}$ , the variational formulation of (1) reads:  
 $\forall t \in (0, T]$  find  $\mathbf{u} = \mathbf{u}(t) \in V$  such that

$$\mathbf{d}_{tt}(\rho \mathbf{u}, \mathbf{v})_\Omega + \mathcal{A}(\mathbf{u}, \mathbf{v})_\Omega = \mathcal{L}(\mathbf{v}), \quad \forall \mathbf{v} \in V, \quad (2)$$

where the bilinear form  $\mathcal{A}(\cdot, \cdot) : V \times V \rightarrow \mathbb{R}^d$  is defined as  $\mathcal{A}(\mathbf{u}, \mathbf{v})_\Omega = (\underline{\sigma}(\mathbf{u}), \underline{\varepsilon}(\mathbf{v}))_\Omega$ , and the linear functional  $\mathcal{L} : V \rightarrow \mathbb{R}^d$  as  $\mathcal{L}(\mathbf{v}) = (\mathbf{t}, \mathbf{v})_{\Gamma_N} + (\mathbf{t}^*, \mathbf{v})_{\Gamma_{NR}} + (\mathbf{f}, \mathbf{v})_\Omega$ . We suppose that the strain tensor  $\underline{\varepsilon}$  and the stress tensor  $\underline{\sigma}$  are related through the Hooke's law

$$\underline{\varepsilon}(\mathbf{u}) = \frac{1}{2}(\nabla \mathbf{u} + \nabla \mathbf{u}^\top), \quad \underline{\sigma}(\mathbf{u}) = \lambda \nabla \cdot \mathbf{u} \mathbf{I} + 2\mu \underline{\varepsilon}(\mathbf{u}),$$

where  $\mathbf{I}$  is the  $d$ -dimensional identity tensor and  $\lambda$  and  $\mu$  are the Lamé elastic coefficients. We remark that for heterogeneous media  $\rho, \lambda$  and  $\mu$  are bounded functions of the spatial variable, not necessarily continuous i.e.,  $\rho, \lambda$  and  $\mu \in L^\infty(\Omega)$ . Finally, to complete problem (2), we prescribe initial conditions  $\mathbf{u}_0$  and  $\mathbf{u}_1$  for the displacement and the velocity, respectively.

It can be proved that the bilinear form  $\mathcal{A}(\cdot, \cdot)$  is symmetric,  $V$ -elliptic and continuous. These conditions imply that problem (2) admits a unique solution, (cf. [4, 23]).

Let  $V_\delta$  be a suitable finite dimensional approximation of the space  $V$ , the semi-discrete approximation of (2) reads :  $\forall t \in (0, T]$  find  $\mathbf{u}_\delta = \mathbf{u}_\delta(t) \in V_\delta$  such that

$$\mathbf{d}_{tt}(\rho \mathbf{u}_\delta, \mathbf{v})_\Omega + \mathcal{A}(\mathbf{u}_\delta, \mathbf{v}) = \mathcal{L}(\mathbf{v}), \quad \forall \mathbf{v} \in V_\delta. \quad (3)$$

In general, in non-conforming approximations, the space  $V_\delta$  is not a subspace of  $V$ . In the following section we describe how to build  $V_\delta$  for both for the Mortar Spectral Element Method (MSEM) and the Discontinuous Galerkin Spectral Element Method (DGSEM).

### 3 NON CONFORMING FORMULATIONS

To approximate the problem (3) we start by a discretization of the spatial differential operators in  $\Omega$ , that rely on a time-independent three-level spatial decomposition of the domain  $\Omega$ .

At the first level, we subdivide  $\Omega$  into  $K$  non overlapping regions  $\Omega_k, k = 1, \dots, K$ , such that  $\bar{\Omega} = \bigcup_{k=1}^K \bar{\Omega}_k$  with  $\Omega_k \cap \Omega_\ell = \emptyset$  if  $k \neq \ell$  and we define the skeleton of this (macro) decomposition as  $\mathcal{S} = \bigcup_{k=1}^K \partial\Omega_k \setminus \partial\Omega$ . Note that this decomposition can be geometrically non-conforming, i.e., for two neighbouring subdomains  $\Omega_k, \Omega_\ell$ , the interface  $\gamma = \partial\Omega_k \cap \partial\Omega_\ell$  may not be a complete side (for  $d = 2$ ) or face (for  $d = 3$ ) of  $\Omega_k$  or  $\Omega_\ell$ .

To get the second level, in each  $\Omega_k$  we introduce a (meso) partitioning  $\mathcal{T}_{h_k}$ , made by elements  $\Omega_k^j$  that are image through an invertible mapping  $F_k^j$  of the reference element  $\hat{\Omega} = (-1, 1)^d$ . The quadrilaterals  $\Omega_k^j$ , if  $d = 2$ , or hexahedra, if  $d = 3$ , have typical linear size  $h_k$  and  $\bar{\Omega}_k = \bigcup_{j=1}^{J_k} \bar{\Omega}_k^j$ .

The third (micro) level is represented by the so-called Gauss-Lobatto-Legendre (GLL) points in each mesh element  $\Omega_k^j$ . Let  $\mathbf{Q}_{N_k}(\hat{\Omega})$  be the space of functions defined on  $\hat{\Omega}$  that are algebraic polynomials of degree less than or equal to  $N_k \geq 2$  in each spatial variable  $x_1, \dots, x_d$ . Thus, we set

$$\mathbf{Q}_{N_k}(\Omega_k^j) = \left\{ v = \hat{v} \circ F_k^{j-1} : \hat{v} \in \mathbf{Q}_{N_k}(\hat{\Omega}) \right\},$$

and we define the finite dimensional space  $X_\delta(\Omega_k)$  as

$$X_\delta(\Omega_k) = \left\{ v_\delta \in \mathcal{C}^0(\overline{\Omega}_k) : v_{\delta|\Omega_k^j} \in \mathbf{Q}_{N_k}(\Omega_k^j) \forall \Omega_k^j \in \mathcal{T}_{h_k} \right\},$$

and finally  $V_\delta = \{ \mathbf{v}_\delta \in [L^2(\Omega)]^d : \mathbf{v}_{\delta|\Omega_k} \in [X_\delta(\Omega_k)]^d \forall k = 1, \dots, K : \mathbf{v}_{\delta|\Gamma_D} = \mathbf{0} \}$ . Here  $\delta = \{ \mathbf{h}, \mathbf{N} \}$  with  $\mathbf{h} = (h_1, \dots, h_K)$  and  $\mathbf{N} = (N_1, \dots, N_K)$  are  $K$ -uplets of discretization parameters. Problem (3) is then equivalent to:  $\forall t \in (0, T]$  find  $(\mathbf{u}_{\delta,1}(t), \dots, \mathbf{u}_{\delta,K}(t)) \in V_\delta$  such that

$$\sum_{k=1}^K d_{tt}(\rho \mathbf{u}_{\delta,k}, \mathbf{v}_k)_{\Omega_k} + \mathcal{A}(\mathbf{u}_{\delta,k}, \mathbf{v}_k)_{\Omega_k} + \mathcal{B}(\mathbf{u}_{\delta,k}, \mathbf{v}_k)_{\partial\Omega_k \setminus \partial\Omega} = \sum_{k=1}^K \mathcal{L}(\mathbf{v}_k)_{\Omega_k}, \quad (4)$$

for all  $(\mathbf{v}_1, \dots, \mathbf{v}_K) \in V_\delta$ , where

$$\mathcal{A}(\mathbf{u}, \mathbf{v})_{\Omega_k} = (\underline{\sigma}(\mathbf{u}), \underline{\varepsilon}(\mathbf{v}))_{\Omega_k}, \quad \text{and} \quad \mathcal{B}(\mathbf{u}, \mathbf{v})_{\partial\Omega_k \setminus \partial\Omega} = (\underline{\sigma}(\mathbf{u}) \cdot \mathbf{n}, \mathbf{v})_{\partial\Omega_k \setminus \partial\Omega}. \quad (5)$$

Depending on the chosen non-conforming approach, the functional space  $V_\delta$  is completed by additional conditions on  $\mathbf{u}_{\delta,k}$ ,  $k = 1, \dots, K$ , on the skeleton of the macro decomposition which ensure that  $\mathbf{u}_{\delta,k}$  is the restriction to  $\Omega_k$  of  $\mathbf{u}_\delta \in H^1(\Omega)^d$ . The bilinear form  $\mathcal{B}(\cdot, \cdot)$  may either be zero or gather all the contributions  $(\sigma(\mathbf{u}_{\delta,k}) \cdot \mathbf{n}_k, \mathbf{v}_k)_{\partial\Omega_k \setminus \partial\Omega}$ ,  $k = 1, \dots, K$ , depending on the chosen approach. Equation (4) represents the starting point to introduce the MSEM and the DGSEM.

In the next sections we describe the two approaches. To ease the presentation, we suppose that  $\Gamma_D = \partial\Omega$  and we assume that each partition  $\mathcal{T}_{h_k}$  of  $\Omega_k$  consists in only one element, i.e.,  $\Omega$  is subdivided into  $K$  non-overlapping spectral elements  $\Omega_1, \dots, \Omega_K$  so that  $\overline{\mathcal{S}} = \bigcap_{k=1}^K \partial\overline{\Omega}_k \setminus \Gamma_D$ . The more general case follows from similar arguments.

### 3.1 Mortar Spectral Formulation

In this section we introduce the MSEM for the solution of (4), see [11, 21] for a more detailed description. We denote by  $\Gamma_k^\ell$ ,  $\ell = 1, \dots, 2d$ , the edges (faces) of each subdomain  $\Omega_k$ ,  $k = 1, \dots, K$ , so that  $\partial\Omega_k = \bigcup_{\ell=1}^{2d} \overline{\Gamma}_k^\ell$ . We then identify the skeleton  $\mathcal{S}$  as the union of elementary non-empty components called *mortars* (or *masters*), more precisely

$$\mathcal{S} = \bigcup_{k=1}^K (\partial\Omega_k \setminus \partial\Omega) = \bigcup_{m=1}^M \overline{\gamma}_m, \quad \text{with } \gamma_m \cap \gamma_n = \emptyset, \quad \text{if } m \neq n, \quad (6)$$

where each mortar is a whole edge (or face)  $\Gamma_{k(m)}^{\ell(m)}$  of a specific element  $\Omega_{k(m)}$  and  $m$  is an arbitrary numbering  $m = 1, \dots, M$ , with  $M$  a positive integer. Those edges or faces  $\Gamma_k^\ell$  that do not coincide with a mortar are called *non-mortars* (or *slaves*) and provide a dual description of the skeleton, as

$$\mathcal{S} = \bigcup_{m \text{ mortar}} \gamma_m^+ = \bigcup_{n \text{ non mortar}} \gamma_n^-.$$

The intersection of the closures of the mortars defines a set of vertices or *cross-points*

$$\mathcal{V} = \{ \mathbf{x}_q = (\overline{\gamma}_r^+ \cap \overline{\gamma}_s^+), \mathbf{x}_q \notin \overline{\gamma}_m^+, m = 1, \dots, M \},$$

where  $q$  is an arbitrary numbering  $q = 1, \dots, V$ . We define as well the set  $\tilde{\mathcal{V}}$  of *virtual vertices* (that are not cross-points) as  $\tilde{\mathcal{V}} = \{ \tilde{\mathbf{x}}_q = (\overline{\gamma}_r^+ \cap \gamma_s^+) \}$ , where  $q$  is an arbitrary numbering

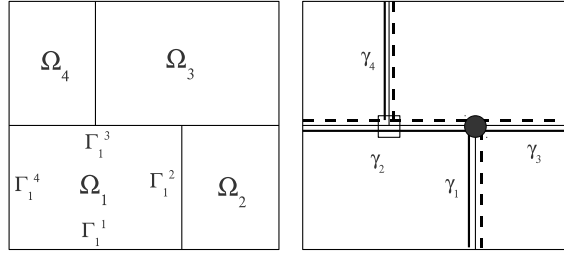


Figure 1: Nonconforming domain decomposition (left) and skeleton structure (right) showing a cross-point ( $\bullet$ ), a virtual vertex ( $\square$ ), the mortars (dark continuous lines) and the non-mortars (dark dashed lines).

$q = 1, \dots, \tilde{\mathcal{V}}$  (see Fig. 1). Let  $\Lambda_\delta(\Gamma_k^\ell) = \mathbf{Q}_{N_k}(\Gamma_k^\ell)$  be the space of the traces of functions of  $X_\delta(\Omega_k)$  over  $\Gamma_k^\ell$  and  $\widehat{\Lambda}_\delta(\Gamma_k^\ell) = \mathbf{Q}_{N_k-2}(\Gamma_k^\ell)$ . We can now define the nonconforming spectral element discretization space  $\tilde{V}_\delta$  as the space of functions  $\mathbf{v}_\delta \in V_\delta$  that satisfy the following additional *mortar matching condition*:

**(MC)** let  $\Phi$  be the *mortar function* associated with  $\mathbf{v}_\delta$ , i.e., a function that is continuous on  $\mathcal{S}$ , zero on  $\partial\Omega$  and such that on each mortar  $\gamma_m = \Gamma_{k(m)}^{\ell(m)}$  coincides with the restriction of  $\mathbf{v}_{\delta,k} = \mathbf{v}_{\delta|\Omega_k}$  to  $\gamma_m$ ; then, for all indices  $(k, \ell)$  such that  $\Gamma_k^\ell$  is contained in  $\mathcal{S}$  but  $(k, \ell) \neq (k(m), \ell(m))$  for all  $m = 1, \dots, M$  (that is for all indices  $(k, \ell)$  such that  $\Gamma_k^\ell$  is a *non-mortar*) we require that:

$$\int_{\Gamma_k^\ell} (\mathbf{v}_{\delta,k} - \Phi) \cdot \hat{\Phi} \, d\gamma = 0 \quad \forall \hat{\Phi} \in [\widehat{\Lambda}_\delta(\Gamma_k^\ell)]^d, \quad (7)$$

and that

$$\mathbf{v}_{\delta|\Omega_k}(\mathbf{x}_q) = \Phi(\mathbf{x}_q), \quad \forall \mathbf{x}_q \in \mathcal{V} \cup \tilde{\mathcal{V}}. \quad (8)$$

The integral matching condition (7) represents a minimization of the jump in functions at internal boundaries with respect to the  $L^2$  norm. The vertex condition (8) ensures exact continuity at cross-points.

The Mortar Spectral Formulation is obtained by solving in each region  $\Omega_k$  the elastodynamic variational problem (4) with homogeneous Neumann boundary conditions on  $\mathcal{S}$  ( $\underline{\sigma}(\mathbf{u}) \cdot \mathbf{n} = \mathbf{0}$  so that  $\sum_k \mathcal{B}(\mathbf{u}, \mathbf{v})_{\partial\Omega_k \setminus \partial\Omega}$  is identically zero), and enforcing weak continuity of the displacement on  $\mathcal{S}$  with *mortar condition* (7). Thus, the semi-discrete Mortar Spectral Formulation reads:

$\forall t \in (0, T]$  find  $(\mathbf{u}_{\delta,1}(t), \dots, \mathbf{u}_{\delta,K}(t)) \in V_\delta^{\text{mortar}}$  such that

$$\sum_k d_{tt}(\rho \mathbf{u}_{\delta,k}, \mathbf{v}_k)_{\Omega_k} + \mathcal{A}(\mathbf{u}_{\delta,k}, \mathbf{v}_k)_{\Omega_k} = \sum_k \mathcal{L}(\mathbf{v}_k), \quad \forall (\mathbf{v}_1, \dots, \mathbf{v}_K) \in V_\delta^{\text{mortar}}, \quad (9)$$

where  $V_\delta^{\text{mortar}} = \{(\mathbf{v}_1, \dots, \mathbf{v}_K) \in V_\delta : \text{the mortar condition (MC) is satisfied}\}$ .

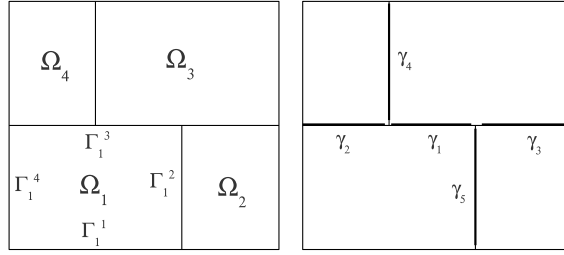


Figure 2: Nonconforming domain decomposition (left) and skeleton structure (right) showing the elementary components (dark continuous lines).

### 3.2 Discontinuous Galerkin Spectral Formulation

In order to introduce the Discontinuous Galerkin Spectral Formulations, we subdivide the skeleton  $\mathcal{S}$  in the set of elementary components (edges if  $d = 2$ , faces if  $d = 3$ ) as follows:

$$\overline{\mathcal{S}} = \bigcup_{j=1}^M \overline{\gamma}_j, \quad \text{with } \gamma_i \cap \gamma_j = \emptyset, \quad \text{if } i \neq j, \quad (10)$$

where each edge (face) is given by  $\overline{\gamma}_j = (\partial\overline{\Omega}_{k(j)} \cap \partial\overline{\Omega}_{\ell(j)}) \setminus \partial\Omega$ , for some different positive integers  $k$  and  $\ell$ . Notice that this decomposition is unique (see Fig. 2). Next, we collect all the edges (faces) in the set  $\mathcal{F}_I$ . For regular enough functions, we use the standard notation [2] to define the jumps ( $[[\cdot]]$ ) and the average ( $\{\cdot\}$ ) operators on each edge (face)  $\gamma \in \mathcal{F}_I$ .

We obtain the following semi-discrete DG Spectral Formulation:

$\forall t \in (0, T]$  find  $\mathbf{u}_\delta = (\mathbf{u}_{\delta,1}(t), \dots, \mathbf{u}_{\delta,K}(t)) \in V_\delta^{DG} \equiv V_\delta$  such that

$$\sum_{k=1}^K (d_{tt}(\rho \mathbf{u}_\delta, \mathbf{v})_{\Omega_k} + \mathcal{A}(\mathbf{u}_\delta, \mathbf{v})_{\Omega_k}) + \sum_{j=1}^M \mathcal{B}(\mathbf{u}_\delta, \mathbf{v})_{\gamma_j} = \mathcal{L}(\mathbf{v}) \quad \forall \mathbf{v} = (\mathbf{v}_1, \dots, \mathbf{v}_K) \in V_\delta^{DG}, \quad (11)$$

with

$$\mathcal{B}(\mathbf{u}_\delta, \mathbf{v})_{\gamma_j} = -(\{\underline{\sigma}(\mathbf{u}_\delta)\}, [[\mathbf{v}]])_{\gamma_j} + \theta ([[ \mathbf{u}_\delta ]], \{\underline{\sigma}(\mathbf{v})\})_{\gamma_j} + \eta_{\gamma_j} ([[ \mathbf{u}_\delta ]], [[ \mathbf{v} ]])_{\gamma_j}. \quad (12)$$

Here  $\eta_{\gamma_j} = \frac{\alpha N_j^2}{h_j} \{\lambda + 2\mu\}_A$ , where  $\{\cdot\}_A$  represents the harmonic average,  $N_j = \max(N_{k(j)}, N_{\ell(j)})$ ,  $h_j = \min(h_{k(j)}, h_{\ell(j)})$  and  $\alpha$  is a positive constant at our disposal. Corresponding to different values of  $\theta$  we obtain different DG schemes, namely:  $\theta = -1$  (resp.  $\theta = 1$ ) leads to the symmetric (resp. non-symmetric) interior penalty method, while  $\theta = 0$  corresponds to the so-called incomplete interior penalty method (see [2, 24, 25, 26] for more details).

## 4 ALGEBRAIC FORMULATION AND TIME INTEGRATION SCHEME

We discuss here the algebraic formulation of the two non-conforming approaches presented in the previous section. In particular we described how to build the linear systems coming from the mortar or DG discretization and discuss the time integration scheme.

#### 4.1 Algebraic formulation of the problem

We denote by  $D = \sum_{k=1}^K (N_k + 1)^2$  the dimension of each component of  $V_\delta$  and we introduce a basis  $\{\Psi_i^1, \Psi_i^2\}_{i=1}^D$  for the finite dimensional space  $V_\delta$ , where  $\Psi_i^1 = (\Psi_i^1, 0)^\top$  and  $\Psi_i^2 = (0, \Psi_i^2)^\top$ . We choose the set of shape functions in such a way that they are orthonormal with respect to the  $L^2$  inner product on the reference element.

We denote by  $\{\mathbf{p}_j\}_{j=1}^D$  the GLL nodes of the mesh and we suppose that  $\Psi_i^1(\mathbf{p}_j) = \Psi_i^2(\mathbf{p}_j) = \delta_{ij}$ , for  $i, j = 1, \dots, D$ , where  $\delta_{ij}$  represents the Kronecker symbol. Dropping the subscript  $\delta$ , we write the trial functions  $\mathbf{u} \in V_\delta$  as a linear combination of the basis functions

$$\mathbf{u}(\mathbf{x}, t) = \sum_{j=1}^D \begin{bmatrix} \Psi_j^1(\mathbf{x}) \\ 0 \end{bmatrix} U_j^1(t) + \sum_{j=1}^D \begin{bmatrix} 0 \\ \Psi_j^2(\mathbf{x}) \end{bmatrix} U_j^2(t).$$

Next, we define  $a_k = 1 + \sum_{j=1}^{k-1} (N_j + 1)^2$  and  $b_k = \sum_{j=1}^k (N_j + 1)^2$  and we order the basis functions such that

$$\mathbf{u}|_{\Omega_k} = (u^1, u^2)|_{\Omega_k}^\top = \left( \sum_{j=a_k}^{b_k} \Psi_j^1 U_{j,k}^1, \sum_{j=a_k}^{b_k} \Psi_j^2 U_{j,k}^2 \right)^\top, \quad \text{for } k = 1, \dots, K.$$

With such a notation (11) can be rewritten as the following set of ODE

$$\begin{bmatrix} \underline{\mathbf{M}}^1 & \underline{\mathbf{0}} \\ \underline{\mathbf{0}} & \underline{\mathbf{M}}^2 \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{U}}^1 \\ \ddot{\mathbf{U}}^2 \end{bmatrix} + \begin{bmatrix} \underline{\mathbf{A}}^1 + \underline{\mathbf{B}}^1 & \underline{\mathbf{A}}^2 + \underline{\mathbf{B}}^2 \\ \underline{\mathbf{A}}^3 + \underline{\mathbf{B}}^3 & \underline{\mathbf{A}}^4 + \underline{\mathbf{B}}^4 \end{bmatrix} \begin{bmatrix} \mathbf{U}^1 \\ \mathbf{U}^2 \end{bmatrix} = \begin{bmatrix} \mathbf{F}^{ext,1} \\ \mathbf{F}^{ext,2} \end{bmatrix}, \quad (13)$$

where  $\ddot{\mathbf{U}}$  represents the vector of the nodal acceleration and  $\mathbf{F}^{ext}$  the vector of externally applied loads. As a consequence of our assumptions on the basis functions, the mass matrices  $\underline{\mathbf{M}}^1$  and  $\underline{\mathbf{M}}^2$  have a block diagonal structure, i.e.,  $\underline{\mathbf{M}}^\ell = \text{diag}(\underline{\mathbf{M}}_1^\ell, \underline{\mathbf{M}}_2^\ell, \dots, \underline{\mathbf{M}}_K^\ell)$ , for  $\ell = 1, 2$ , where each block  $\underline{\mathbf{M}}_k^\ell$  is associated to the spectral element  $\Omega_k$  and  $\underline{\mathbf{M}}_k^\ell(i, j) = (\rho \Psi_j^\ell, \Psi_i^\ell)_{\Omega_k}$ , for  $i, j = a_k, \dots, b_k$ . The matrix  $\underline{\mathbf{A}}$  associated to the bilinear form  $\mathcal{A}(\cdot, \cdot)$  defined in (5) takes the form

$$\underline{\mathbf{A}} = \begin{bmatrix} \underline{\mathbf{A}}^1 & \underline{\mathbf{A}}^2 \\ \underline{\mathbf{A}}^3 & \underline{\mathbf{A}}^4 \end{bmatrix},$$

where the block diagonal matrices  $\underline{\mathbf{A}}^\ell$ ,  $\ell = 1, \dots, 4$  are equal to  $\underline{\mathbf{A}}^\ell = \text{diag}(\underline{\mathbf{A}}_1^\ell, \underline{\mathbf{A}}_2^\ell, \dots, \underline{\mathbf{A}}_K^\ell)$ . The elements of the matrices  $\underline{\mathbf{A}}_k^\ell$ ,  $\ell = 1, \dots, 4$  and  $k = 1, \dots, K$ , are defined by

$$\underline{\mathbf{A}}_k^1(i, j) = \mathcal{A}(\underline{\sigma}(\Psi_j^1), \underline{\varepsilon}(\Psi_i^1))_{\Omega_k}, \quad \underline{\mathbf{A}}_k^2(i, j) = \mathcal{A}(\underline{\sigma}(\Psi_j^2), \underline{\varepsilon}(\Psi_i^1))_{\Omega_k}, \quad \text{for } i, j = a_k, \dots, b_k,$$

$$\underline{\mathbf{A}}_k^3(i, j) = \mathcal{A}(\underline{\sigma}(\Psi_j^1), \underline{\varepsilon}(\Psi_i^2))_{\Omega_k}, \quad \underline{\mathbf{A}}_k^4(i, j) = \mathcal{A}(\underline{\sigma}(\Psi_j^2), \underline{\varepsilon}(\Psi_i^2))_{\Omega_k}, \quad \text{for } i, j = a_k, \dots, b_k.$$

We remark that the matrices  $\underline{\mathbf{M}}$  and  $\underline{\mathbf{A}}$  are very similar to those coming from the discretization of the elastodynamic equation (2) with the conforming Spectral Element Method (see [6, 7]).

If we are using the mortar formulation, the matrix  $\underline{\mathbf{B}}$ , associated to the bilinear form  $\mathcal{B}(\cdot, \cdot)$  defined in (5), is the null matrix, whereas in the DG approach, is the one that takes into account of the discontinuity of the numerical solution across the skeleton  $\mathcal{S}$ . More precisely,

$$\underline{\mathbf{B}} = \begin{bmatrix} \underline{\mathbf{B}}^1 & \underline{\mathbf{B}}^2 \\ \underline{\mathbf{B}}^3 & \underline{\mathbf{B}}^4 \end{bmatrix}, \quad (14)$$

where

$$\underline{\mathbf{B}}^\ell = \begin{bmatrix} \underline{\mathbf{B}}_{1,1}^\ell & \cdots & \underline{\mathbf{B}}_{1,K}^\ell \\ \vdots & \ddots & \vdots \\ \underline{\mathbf{B}}_{K,1}^\ell & \cdots & \underline{\mathbf{B}}_{K,K}^\ell \end{bmatrix}, \quad \text{for } \ell = 1, \dots, 4.$$

In particular the elements of each block  $\underline{\mathbf{B}}_{k,n}^1(i, j) = \sum_{\gamma \in \mathcal{F}_I} \mathcal{B}(\Psi_j^1, \Psi_i^1)_\gamma$ ,  $i = a_k, \dots, b_k$  and  $j = a_n, \dots, b_n$ . The elements of the matrices  $\underline{\mathbf{B}}_{k,n}^\ell$ , for  $\ell = 2, 3, 4$  are defined in a similar way.

The situation is a little bit more complicated in the Mortar approach, since the weak continuity condition across the skeleton  $\mathcal{S}$  does not appear explicitly in the variational equation but it is a constraint in the functional space  $V_\delta^{mortar}$ .

To take into account the **(MC)** we have to modify the system (13) as follows. Without loss of generality let us suppose that  $\gamma_n^-$  is a non mortar edge contained in  $\mathcal{S}$  and that it is shared by two regions  $\Omega_m$  and  $\Omega_n$ . We call *master* the side of  $\gamma_n^-$  belonging to  $\overline{\Omega}_m$  and *slave* the other side. Thus, the *mortar conditions* can be recast as:

(i)  $\Phi = \mathbf{u}_m$  on  $\gamma_n^-$ ,

(ii)  $\int_{\gamma_n^-} (\mathbf{u}_n - \mathbf{u}_m) \cdot \hat{\Phi} ds = 0 \quad \forall \hat{\Phi} \in [\hat{\Lambda}_\delta(\gamma_n^-)]^d$ .

At the algebraic level, the condition in (ii) is represented by the following linear system of equations

$$\begin{bmatrix} \underline{\mathbf{R}}^1 & \underline{\mathbf{0}} \\ \underline{\mathbf{0}} & \underline{\mathbf{R}}^2 \end{bmatrix} \begin{bmatrix} \mathbf{U}_n^1 \\ \mathbf{U}_n^2 \end{bmatrix} = \begin{bmatrix} \underline{\mathbf{P}}^1 & \underline{\mathbf{0}} \\ \underline{\mathbf{0}} & \underline{\mathbf{P}}^2 \end{bmatrix} \begin{bmatrix} \mathbf{U}_m^1 \\ \mathbf{U}_m^2 \end{bmatrix}, \quad (15)$$

where

$$\underline{\mathbf{R}}^\ell(i, j) = \int_{\gamma_n^-} \Psi_j^\ell \hat{\Phi}_i^\ell ds \quad \text{and} \quad \underline{\mathbf{P}}^\ell(i, j) = \int_{\gamma_n^-} \Phi_j^\ell \hat{\Phi}_i^\ell ds, \quad \ell = 1, 2. \quad (16)$$

By using that the shape functions are orthonormal on the reference element and suitable quadrature rules to integrate (16), (cf. [3, 11]), it is possible to easily invert the matrix  $\underline{\mathbf{R}}$  and to reduce (15) to

$$\begin{bmatrix} \mathbf{U}_n^1 \\ \mathbf{U}_n^2 \end{bmatrix} = \begin{bmatrix} \underline{\mathbf{Q}}_n & \underline{\mathbf{0}} \\ \underline{\mathbf{0}} & \underline{\mathbf{Q}}_n \end{bmatrix} \begin{bmatrix} \mathbf{U}_m^1 \\ \mathbf{U}_m^2 \end{bmatrix},$$

where  $\underline{\mathbf{Q}}_n = (\underline{\mathbf{R}}^1)^{-1} \underline{\mathbf{P}}^1 = (\underline{\mathbf{R}}^2)^{-1} \underline{\mathbf{P}}^2$ . To obtain a global projection operator  $\tilde{\mathbf{Q}}$  we proceed as follows. For each component of  $\mathbf{u}$  we denote by  $\mathbf{U}_{slave}$  the vector of unknowns associated to the dofs that lay on the slave side of  $\mathcal{S}$  and by  $\mathbf{U}_{master}$  the vector of unknowns associated to all the remaining dofs. Then, for each  $\gamma_n^-$  contained into the skeleton  $\mathcal{S}$  we build the local projection operator  $\underline{\mathbf{Q}}_n$  and we store it into the matrix  $\tilde{\mathbf{Q}}$ . In this way  $\tilde{\mathbf{Q}}$  has a block structure of the form

$$\tilde{\mathbf{Q}} = \begin{bmatrix} \hat{\mathbf{Q}} & \underline{\mathbf{0}} \\ \underline{\mathbf{0}} & \hat{\mathbf{Q}} \end{bmatrix}, \quad (17)$$

where  $\hat{\mathbf{Q}}$  is block diagonal matrix with a block equal to the identity and the other equal to the rectangular matrix  $\underline{\mathbf{Q}}$  containing all the local matrices  $\underline{\mathbf{Q}}_n$ . Thus, we have that the global linear system can be expressed as

$$\tilde{\mathbf{Q}}^\top \tilde{\mathbf{M}} \tilde{\mathbf{Q}} \tilde{\mathbf{U}}_{master} + \tilde{\mathbf{Q}}^\top \tilde{\mathbf{A}} \tilde{\mathbf{Q}} \tilde{\mathbf{U}}_{master} = \tilde{\mathbf{Q}}^\top \mathbf{F}^{ext}, \quad (18)$$

where the rows and the columns of the matrices  $\tilde{\mathbf{M}}$  and  $\tilde{\mathbf{A}}$  have been modified according to these latter assumptions on the unknown renumbering. We remark that it is possible to obtain



the linear system (18) using as a basis for  $V_\delta^{mortar}$ , the functions  $\{\tilde{\Psi}_i^1, \tilde{\Psi}_i^2\}_{i=1}^D$ , where  $\tilde{\Psi}_i^1 = (\tilde{\Psi}_i^1, 0)^\top$  and  $\tilde{\Psi}_i^2 = (0, \tilde{\Psi}_i^2)^\top$  are defined by

$$\tilde{\Psi}_i^\ell = \begin{cases} \Psi_i^\ell & \forall i \text{ s.t } \mathbf{p}_i \text{ is a master node,} \\ \sum_j \hat{Q}_{ij} \Psi_j^\ell & \forall i \text{ s.t } \mathbf{p}_i \text{ is a slave node, } (\mathbf{p}_j \text{ master node on } \mathcal{S}). \end{cases}$$

All the terms appearing in the algebraic formulations presented so fare are computed using the Gauss-Lobatto quadrature rule in which the quadrature points coincide with GLL points. We notice that since the term  $\Psi_j \Psi_i \in \mathbf{Q}_{2N_k}$ , for some  $k$ , the spectral mass matrix is slightly under integrated. However, since the Gauss-Lobatto rule with  $N_k$  points is exact for polynomials up to degree  $2N_k - 1$ , the final accuracy of spectral methods is not damaged [6].

Finally, we point out that if  $\mathbf{f}^{visc} \neq 0$  we must compute the following additional external forces:

$$\begin{bmatrix} \mathbf{F}^{visc,1} \\ \mathbf{F}^{visc,2} \end{bmatrix} = - \begin{bmatrix} \underline{\mathbf{C}}^1 & \underline{\mathbf{0}} \\ \underline{\mathbf{0}} & \underline{\mathbf{C}}^2 \end{bmatrix} \begin{bmatrix} \dot{\mathbf{U}}^1 \\ \dot{\mathbf{U}}^2 \end{bmatrix} - \begin{bmatrix} \underline{\mathbf{D}}^1 & \underline{\mathbf{0}} \\ \underline{\mathbf{0}} & \underline{\mathbf{D}}^2 \end{bmatrix} \begin{bmatrix} \mathbf{U}^1 \\ \mathbf{U}^2 \end{bmatrix},$$

where the matrices  $\underline{\mathbf{C}}^\ell$  and  $\underline{\mathbf{D}}^\ell$ , for  $\ell = 1, 2$  have a block diagonal structure. Each block  $\underline{\mathbf{C}}_k^\ell$  and  $\underline{\mathbf{D}}_k^\ell$  is associated to the spectral element  $\Omega_k$  and

$$\mathbf{C}_k^\ell(i, j) = (\rho\zeta \Psi_j^\ell, \Psi_i^\ell)_{\Omega_k}, \quad \mathbf{D}_k^\ell(i, j) = (\rho\zeta^2 \Psi_j^\ell, \Psi_i^\ell)_{\Omega_k}, \quad \text{for } i, j = a_k, \dots, b_k,$$

respectively. Then the discretized system becomes:

$$\underline{\mathbf{M}}\ddot{\mathbf{U}} + \underline{\mathbf{C}}\dot{\mathbf{U}} + (\underline{\mathbf{A}} + \underline{\mathbf{B}} + \underline{\mathbf{D}})\mathbf{U} = \mathbf{F}^{ext}, \quad (19)$$

where the accelerations  $\ddot{\mathbf{U}}$  and the velocities  $\dot{\mathbf{U}}$  are approximated as described in the next section.

## 4.2 Time integration

Let now subdivide into  $N$  subinterval of amplitude  $\Delta t = \frac{T}{N}$  the interval  $(0, T]$ : the time integration scheme for (13) is achieved with the second order central difference scheme, setting  $t_n = n\Delta t$ :

$$\ddot{\mathbf{U}}(t_n) = \frac{\mathbf{U}(t_{n+1}) - 2\mathbf{U}(t_n) + \mathbf{U}(t_{n-1}))}{\Delta t^2}, \quad \dot{\mathbf{U}}(t_n) = \frac{\mathbf{U}(t_{n+1}) - \mathbf{U}(t_{n-1}))}{2\Delta t}. \quad (20)$$

Thus, the equation (13) or (18) at each time step  $t_n$  becomes:

$$\underline{\mathbf{K}}\mathbf{U}(t_{n+1}) = \mathbf{b}(\mathbf{U}(t_n), \mathbf{U}(t_{n-1}), \mathbf{F}^{ext}(t_n), \underline{\mathbf{A}}, \underline{\mathbf{B}}), \quad (21)$$

with initial condition  $\mathbf{U}(t_0) = \mathbf{u}_0$  and  $\dot{\mathbf{U}}(t_0) = \mathbf{u}_1$ . If we adopt a fully explicit time integration scheme the matrix  $\underline{\mathbf{K}}$  is the mass matrix, i.e.  $\underline{\mathbf{K}} = \underline{\mathbf{M}}$ , if a DGSEM is employed and  $\underline{\mathbf{K}} = \tilde{\mathbf{Q}}^\top \tilde{\mathbf{M}} \tilde{\mathbf{Q}}$  for the MSEM. In particular, for the latter approach, taking advantage of the structure of  $\tilde{\mathbf{Q}}$  it is possible to decompose the linear system (21) as follows

$$\begin{bmatrix} \underline{\mathbf{M}}_{master} & 0 \\ 0 & \underline{\mathbf{Q}}^\top \underline{\mathbf{M}}_{slave} \underline{\mathbf{Q}} \end{bmatrix} \begin{bmatrix} \mathbf{U}_{master}^{\mathcal{I}} \\ \mathbf{U}_{master}^{\mathcal{S}} \end{bmatrix} = \begin{bmatrix} \mathbf{b}_{master}^{\mathcal{I}} \\ \underline{\mathbf{Q}}^\top \mathbf{b}_{slave}^{\mathcal{S}} \end{bmatrix}. \quad (22)$$

Here the superscripts  $\mathcal{I}$  and  $\mathcal{S}$  denote if the unknowns belong to the interior or to the skeleton of the domain. Then at each time step we solve separately the two blocks of the linear systems (22).

In particular for the non diagonal block we perform the LU-factorization with pivoting (cf [22]). To ensure stability, the explicit time integration scheme must satisfy the usual Courant-Friedrichs-Levy (CFL) condition (see [22]) that imposes a restriction on the amplitude of  $\Delta t$ . This limitation is proportional to the minimal distance  $\Delta x$  between two consecutive spectral nodes  $\mathbf{p}_i$  and  $\mathbf{p}_j$ , with  $i \neq j$ , of the numerical grid, see [8]. Since GLL points are clustered near the edges of spectral elements  $\Omega_k$ , where the grid size is proportional to  $N_k^{-2}$ , the stability requirement on  $\Delta t$  may become too restrictive for very large approximation orders  $N_k$ . In such cases an implicit time scheme is recommended.

## 5 HOW IMPLEMENTING THE METHODS

In this section we describe the implementation of the MSEM and the DGSEM in the spectral element code GeoELSE [14] and we compare the two different algorithms from the efficiency view point. In this context the word "efficiency" has the meaning of low memory storage and executing program velocity. In this sense, the assembling of the matrices in (13)-(18) is performed once, outside the time loop.

After setting the initial condition  $\mathbf{u}_0$  and  $\mathbf{u}_1$ , we build the skeleton  $\mathcal{S}$  as explained in (6)-(10) for the MSEM or the DGSEM respectively. In the mortar solution scheme, see Algorithm 1, a further step is required in order to identify the *master* and the *slave* decomposition of  $\mathcal{S}$ .

For both algorithms we notice that in general, all the matrix-vector multiplications involving  $\underline{\mathbf{M}}$ ,  $\underline{\mathbf{A}}$ ,  $\underline{\mathbf{B}}$  and  $\underline{\mathbf{Q}}$  have to be intended subdomains per subdomains.

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### Algorithm 1: Mortar Solution Scheme

1. Set initial conditions  $\mathbf{u}_0$  and  $\mathbf{u}_1$ .
  2. Build the skeleton  $\mathcal{S}$  for the domain  $\Omega$ .
  3. Decompose  $\mathcal{S}$  into the union of *master* and *slave* edges.
  4. Construct the projection operator  $\underline{\mathbf{Q}}$  for the interface unknowns  $\mathbf{U}_{slave}$ .
  5. Perform the LU-factorization of  $\underline{\mathbf{Q}}^\top \underline{\mathbf{M}}_{slave} \underline{\mathbf{Q}}$ .
  6. For each discrete time  $t_n$ :
    - compute the internal forces  $\mathbf{F}^{int}(t_n) = \underline{\mathbf{A}}\mathbf{U}(t_n)$ ;
    - assemble external forces  $\mathbf{F}^{ext}(t_n)$ ;
    - solve for the *master* unknowns  $\mathbf{U}_{master}$  the systems (22);
    - perform the projection on the *slave* unknowns;
    - if the final time  $T$  is not reached set  $t_n \leftarrow t_{n+1}$  and go to 6.
- 

Algorithm 2 describes the DG solution scheme. Here we denote by  $\mathbf{J}(t_n) = \underline{\mathbf{B}}\mathbf{U}(t_n)$  the vector containing the interface terms. Since the matrix  $\underline{\mathbf{B}}$  defined in (14) has a highly sparsity structure, it is stored taking advantage of it.

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### Algorithm 2: DG Solution Scheme

1. Set initial conditions  $\mathbf{u}_0$  and  $\mathbf{u}_1$ .
2. Build the skeleton  $\mathcal{S}$  for the domain  $\Omega$ .

3. Decompose  $\mathcal{S}$  into elementary components.
4. Construct the matrix  $\underline{\mathbf{B}}$  for the interface unknowns.
5. For each discrete time  $t_n$ :
  - compute the internal forces  $\mathbf{F}^{int}(t_n) = \underline{\mathbf{A}}\mathbf{U}(t_n)$ ;
  - assemble external forces  $\mathbf{F}^{ext}(t_n)$ ;
  - compute the jumps at the interfaces  $\mathbf{J}(t_n) = \underline{\mathbf{B}}\mathbf{U}(t_n)$ ;
  - solve the system  $\underline{\mathbf{M}}\ddot{\mathbf{U}} = \mathbf{F}^{ext}(t_n) - \mathbf{F}^{int}(t_n) - \mathbf{J}(t_n)$ ;
  - if the final time  $T$  is not reached set  $t_n \leftarrow t_{n+1}$  and go to 4.

According to [1, 9, 10], it seems that for elastic wave propagation problems the more effective method, in term of accuracy, grid dispersion and stability is the symmetric interior penalty Galerkin method (SIPG). However, if the symmetric approach is used we recall that the constant  $\alpha$  in (12) must be sufficiently large to guarantee consistency of the method without affecting the conditioning of the stiffness matrix in (13).

## 6 A SOIL-STRUCTURE INTERACTION PROBLEM

In this section we aim at studying a soil-structure interaction problem, namely the seismic response of a railway viaduct (Acquasanta viaduct, Genova, Italy). We consider the viscoelastic model (1) in the computational domain  $(x, z) \in \Omega = (0, 10^4m) \times (0, f(x))$ , where  $f$  describes the top profile of the bridge and of the surrounding valley, see Fig. 3. The size of the domain is chosen in order to avoid any possible interference with reflections of the waves of interest with the spurious ones eventually arising from the absorbing boundaries. The dynamic and mechanical properties of the structure and of the surrounding soil are summarized in Table 6. Depending on the material involved, we subdivided the computational grid into different regions, as shown in Fig. 3 (top panel). Note that the mesh was designed to propagate up to about 3 Hz.

We simulate a point source load of the form  $\mathbf{f}(\mathbf{x}, t) = \mathbf{g}(\mathbf{x})h(t)$ , where  $\mathbf{f}$  is the external force introduced in (1). The function  $\mathbf{g}$  describes the space distribution of the source and often is the body force  $\mathbf{g}(\mathbf{x}) = \delta(\mathbf{x} - \mathbf{x}_S)\hat{\mathbf{w}}$ , where  $\delta$  represents the Dirac distribution,  $\mathbf{x}_S$  is the source location and  $\hat{\mathbf{w}}$  is the direction of the body force. The source time history is given by a Ricker-type time function with maximum frequency  $\nu_{max} = 3Hz$ , defined as

$$h(t) = h_0[1 - 2\beta(t - t_0)^2] \exp[-\beta(t - t_0)^2], \quad (23)$$

where  $h_0$  is a scale factor,  $t_0 = 2$  seconds is the time shift and  $\beta = \pi^2\nu_{max}^2 = 9.8696 s^{-1}$  is a parameter that determines the width of the wavelet (23).

In Fig. 3 we show the two different computational grids used for the numerical simulations. The conforming grid, Fig. 3 left, is used with SEM discretization to produce a reference solution for the problem. It provides, in fact, a sufficiently accurate discretization, as we verified that further mesh refinements generates quasi-identical seismograms. The non-conforming grid, shown in Fig. 3 right, is used for both DGSEM and MSEM simulations.

In our analysis we choose the polynomial approximation degree as described in Table 6. It is worth highlighting that the non-conforming approximations lead to a dramatic reduction of the size of the numerical model and, hence, of the computational costs (102.640 unknowns for

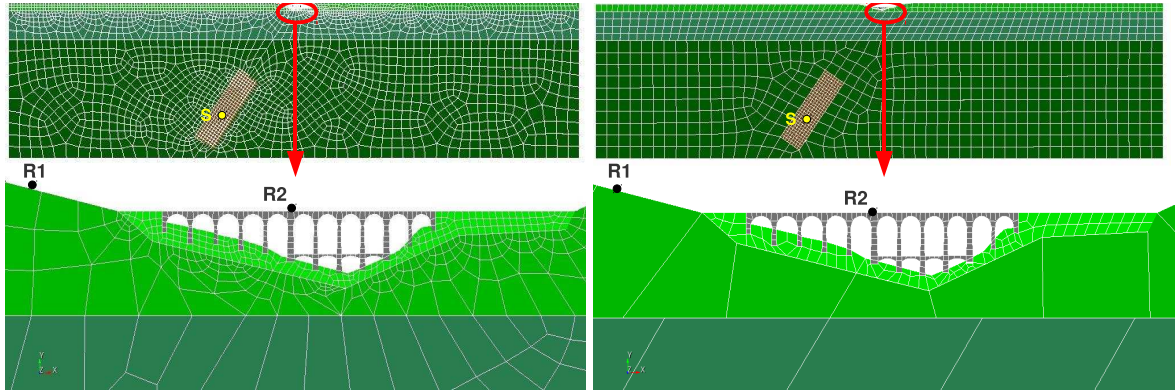


Figure 3: Conforming (left) and non conforming (right) grids. The full domain is displayed on the top and a zoom of the railway bridge is displayed on the bottom. The receivers R1 and R2, on the ground and on the bridge, respectively, are also highlighted.

Layer	$\rho [Kg/m^3]$	$c_P [m/s]$	$c_S [m/s]$	$\zeta [1/s]$	$N [SEM]$	$N [MSEM/DGSEM]$
1 (bridge)	1750	1218	716,7	0.6283	4	2
2 (stiff soil)	2400	1100	635	0.31416	4	2
3 (soft bedrock)	2400	1100	635	0.02513	4	4
4 (medium bedrock)	2600	1700	982	0.02284	4	4
5 (stiff bedrock)	2800	2300	1330	0.02094	4	4
6 (stiff bedrock)	2800	2300	1330	0.02094	4	4

Table 1: Dynamic and mechanical parameters and polynomial approximation degree  $N$  for each subregion of the domain decomposition (the factor  $\zeta$  takes into account the visco-elastic linear soil behavior).

SEM vs. 41.322 for MSEM or DGSEM).

Such an advantage is expected to play a major role for 3D engineering applications. In Fig. 4 (resp Fig. 5 we analyse the synthetic seismograms recorded by the receiver R1 (resp. R2) on the top of the ground (resp. bridge) using the misfits criteria introduced in [19]. The results shown an excellent fit of the data for R1 and a good fit for R2. Probably, for the latter receiver, the results are affected by the grid dispersion phenomenon arising when low order polynomial approximation degrees are used [1, 9, 10].

## 7 CONCLUSIONS

In this paper we compared two different non-conforming high order numerical techniques, namely the Mortar Spectral Element Method and the Discontinuous Galerkin Spectral Element Method, for the approximation of the elastic wave equation in heterogeneous media. The key feature of these methods is to replace the exact continuity condition at the skeleton of the decomposition with a weak one, written in terms of the jumps of the displacements and the tractions across the interfaces. Relaxing the continuity condition is then possible, preserving the accuracy of high order methods, to deal with a geometrically non-conforming domain partitions where local meshes are independently generated from the neighbouring ones and associated with different spectral approximation degrees. Note that the subdomain partition is constructed according to the (available) material properties. Starting from a common weak formulation we describe both approaches in parallel in order to highlight their analogies and their differences. We gave a special attention to the implementation aspects of the two techniques in order to make the reader able to deal with an efficient numerical coding. Finally, we show that the MSEM and the DGSEM can be effectively used for complex seismic wave propagation problems, namely the soil-structure interaction between a valley and a railway bridge. The results, compared with those obtained with the SEM, show that both the non-conforming strategies are good in term of accuracy and computational effort. We refer to [1] for the full comparison of the methods in term of convergence, accuracy, grid dispersion and stability.

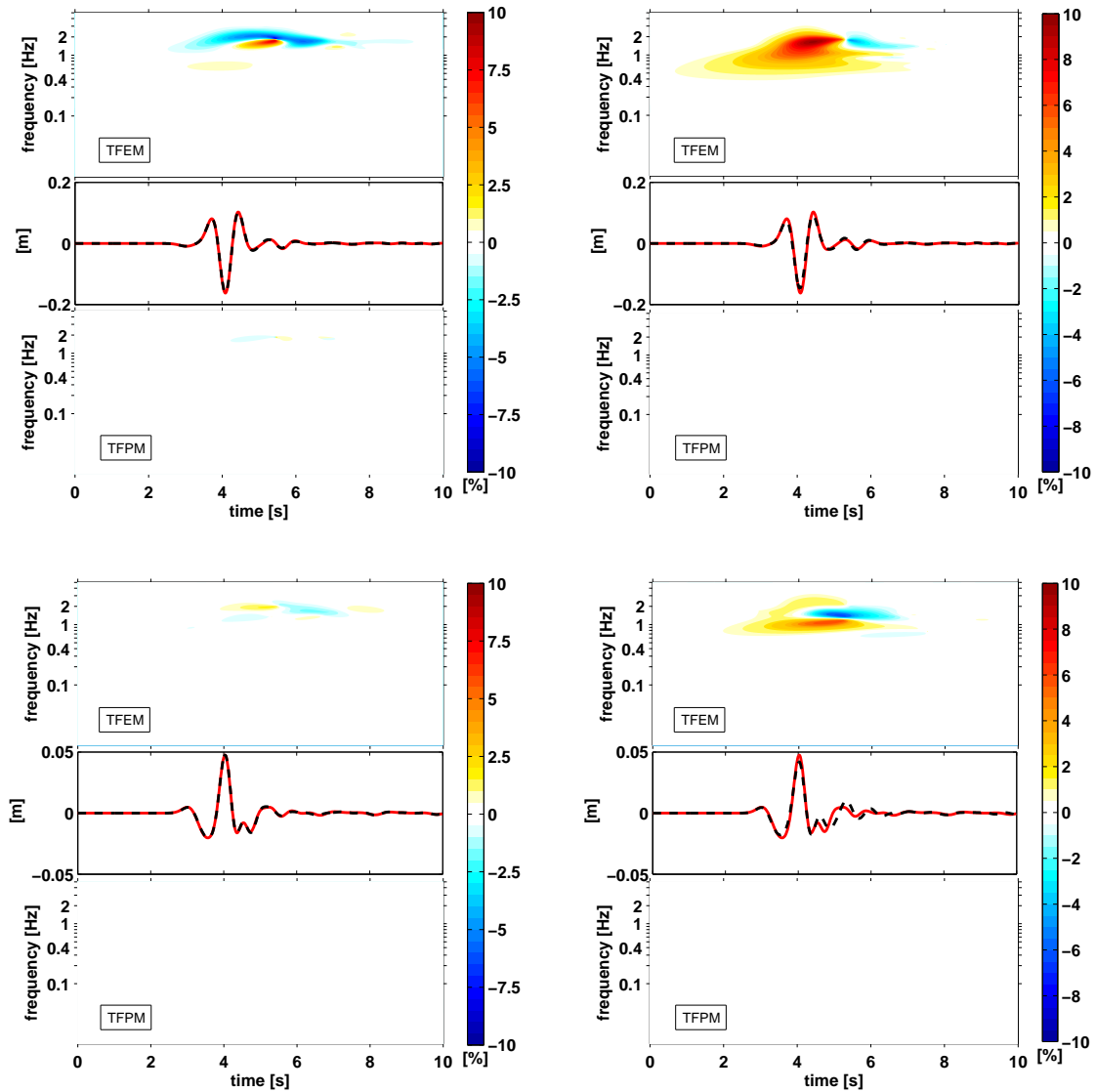


Figure 4: Analysis of the synthetic signals recorded by receiver R1, using the misfits criteria described in [19]. Comparison between the synthetic seismograms obtained with SEM and DGSEM (left) and SEM and MSEM (right). The graphics are subdivided as follows. Middle: displacement obtained using conforming (solid line) and non-conforming (dashed line) approximations. TFEM: time frequency envelope misfits. TFPM: time frequency phase misfits. Top: horizontal component. Bottom: vertical component.

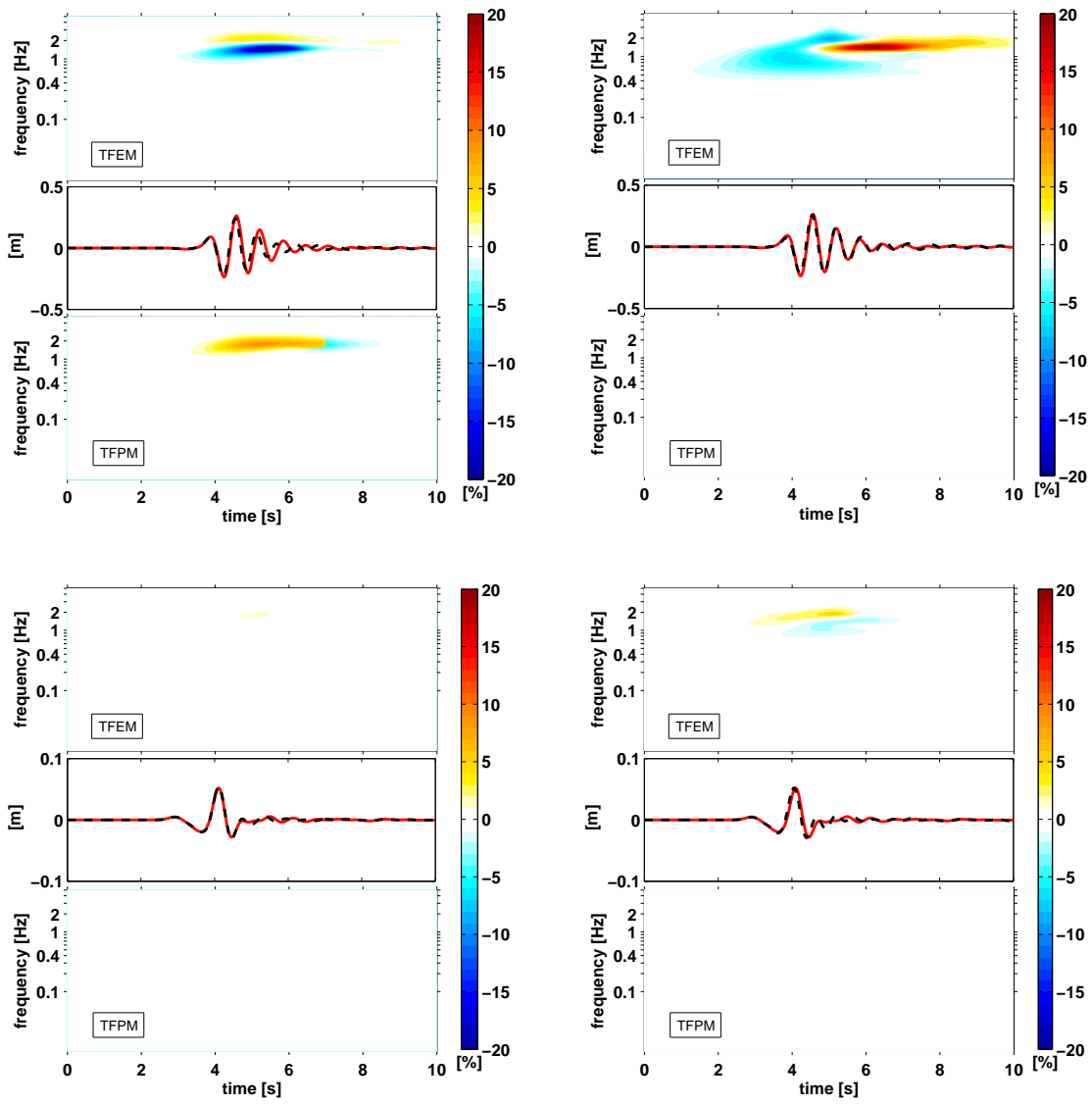


Figure 5: As in Fig. 4 but for receiver R2.

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