

Long duration, high altitude, super pressure balloons; Design considerations and advances in analytical support

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Abstract

Long duration, high altitude pressurized balloons, often colloquially referred to as ‘pumpkin’ balloons, have uses in the fields of scientific or meteorological research, telecommunications and recreation. Whilst the overall structural system of these balloons is easily described, subtleties of performance as a consequence of the visco-elastic nature of the balloon envelope, the large temperature delta from manufacture to deployment, the interface between the film and tendon and susceptibility to instability, make the detailed design of these balloons far from straightforward.

Tensys have been involved in the numerical form finding and load analysis of architectural stressed membrane structures for almost thirty years using their in-house Finite Element (FE) software suite, inTENS [1-3]. Tensys Dynamics Ltd (TDL) was formed in 2004 to provide a similar consultancy service for the aerospace industry. TDL has been providing analytical support to various ‘pumpkin’ balloon programs for 15 years.

The paper will introduce this form of balloon in terms of overall geometry, uses and the basic structural system. Balloon construction and the early problems of geometric and deployment instability will be briefly reviewed [4-10]. A typical design process [11-12] will be described from the context of the analytical support. Both the capabilities of inTENS and the fidelity of the FE models have improved over time to keep pace with balloon design developments and program requirements [13-15]. Extensive smaller FE models have also been developed and analysed to examine particular local phenomena witnessed in flight or to support investigations into potential failure mechanisms.

The balloon skin is formed from thin polyethylene film, cut into a series of identical strips called ‘gores’, spanning between a braided PBO tendon skeleton. The thorough characterisation of these two component materials is critical to accurate FE modelling. The visco-elastic material model used to represent the film continues to evolve from the original Schapery Rand implementation [16-17] to the current Caltech large strain time dependent model [18-22]. Implementation of the Caltech material model into the inTENS code facilitates time stepping analysis runs.

Balloon programs are supported by a large range of physical tests. These tests vary from small scale uniaxial and biaxial film tests associated with material characterization, tests on local components of a balloon, model balloons up to testing of full scale articles. These tests are typically undertaken at both room and cold temperatures and provide a good opportunity to validate FE analyses.

A major consideration in the design of a pumpkin balloon is the balance of desired stress in the two film directions (meridional and transverse direction). This discussion introduces topics such as global foreshortening (the relative gore / tendon length) and the nature of the interface between the film edge and tendon. The factors affecting the performance of, and developments in the modelling of this interface will be studied.

References

- [1] **WAKEFIELD, DS**, “*Membrane Engineering : Principles and Applications*”, IASS Asia Pacific Conference on Shell and Spatial Structures, Beijing, 1996
- [2] **WAKEFIELD DS**, “*Engineering Analysis of Tension Structures : Theory and Practice*”, Engineering Structures ,Vol 21, pp.680-690, 1999
- [3] **WAKEFIELD, DS**, “*Structures Cladding and Airships*”, Membranes 03: Textile Composites and Inflatable Structures, Barcelona, 2003
- [4] **WAKEFIELD DS**, “*Numerical Modeling of Pumpkin Balloon Instability*”, AIAA 5th ATIO and 16th Lighter-than-Air System Technology and Balloon Systems Conferences ,AIAA-2005-7445, 2005
- [5] **WAKEFIELD DS**, “*Numerical Investigations of Pumpkin Balloon Instability*”, AIAA 19th Aerodynamic Decelerator Systems Technology and Balloon Systems Conference, Williamsburg VA ,AIAA-2007-2604, 2007
- [6] **CALLADINE, CR**, “*Stability of the Endeavour Balloon*”, Buckling of Structures, edited by I Elishakoff et al, Elsevier Science Publishers, 1988
- [7] **NOTT, J**, “*Design Considerations and Practical Results with Long Duration Systems for Manned World Flights*”, Advances in Space Science, Vol.33, pp.1667-1673, 2004
- [8] **DENG, X. and PELLEGRINO, S.**, “*Finite element simulations of clefting in lobed super-pressure balloons,*” AIAA Balloon, Systems Conference, 4-7 May 2009, Seattle, Washington, AIAA-2009-2816.
- [9] **DENG X. & PELLEGRINO S**, “*A technique to predict clefting of lobed super-pressure balloons*”, 11th AIAA ATIO Conference, 20-22 September, Virginia Beach, AIAA-2011-6830,2011
- [10] **PAGITZ M & PELLEGRINO S**, “*Buckling Pressure of ‘Pumpkin’ Balloons*”, International Journal of Solids and Structures, 44(21), 6963-6986, 2007
- [11] **FARLEY RE**, “*BalloonAscent: 3D Simulation Tool for the Ascent and Float of High-Altitude Balloons*”, AIAA 5th ATIO and 16th Lighter-than-Air System Technology and Balloon Systems Conferences ,AIAA-2005-7412, 2005
- [12] **CATHEY H & PIERCE D**, “*Duration Flight of the NASA Super Pressure Balloon*”, AIAA 20th Aerodynamic Decelerator Systems Technology, 18th Lighter-Than-Air Systems Technology and Balloon Systems Conferences, AIAA-2009-2808, 2009
- [13] **WAKEFIELD, DS**, “*Non-Linear Viscoelastic Analysis and the Design of Super-Pressure Balloons: Stress, Strain and Stability*”, AIAA 20th Aerodynamic Decelerator Systems Technology, 18th Lighter-Than-Air Systems Technology and Balloon Systems Conferences, Seattle WA ,AIAA-2009-2813, 2009
- [14] **WAKEFIELD DS**, “*Non-Linear Viscoelastic Analysis and the Design of Super-Pressure Balloons: Stress, Strain and Stability*”, AIAA 20th Aerodynamic Decelerator Systems Technology, 18th Lighter-Than-Air Systems Technology and Balloon Systems Conferences, Seattle WA ,AIAA-2009-2813, 2009
- [15] **WAKEFIELD DS & BOWN AC.**, “*Non-Linear Analysis of the NASA Super Pressure Balloons : Some Detailed Investigations of Recent Antarctic Flight Balloons*”, 11th AIAA ATIO Conference, Virginia Beach, 2011
- [16] **RAND, JL**, “*An Improved Constitutive Model for StratoFilm 420*”, Winzen Engineering Inc. Report, 2008
- [17] **RAND JL**, “*A Nonlinear Plasto-Viscoelastic Constitutive Equation for Balloon Films*”, AIAA 20th Aerodynamic Decelerator Systems Technology, 18th Lighter-Than-Air Systems Technology and Balloon Systems Conferences, AIAA-2009-2812, 2009
- [18] **KWOK K & PELLEGRINO S**, “*Large strain viscoelastic model for balloon film*”, 11th AIAA ATIO Conference, Virginia Beach, AIAA-2011-6939,2011
- [19] **LI J, KWOK K & PELLEGRINO S**, “*Large-Strain Thermoviscoelastic Models for Polyethylene Thin Films*”, Paper submitted for publication.
- [20] **BOSI F. & PELLEGRINO S**, “*Nonlinear thermomechanical response and constitutive modelling of viscoelastic polyethylene membranes*”, Caltech, March 20, 2017
- [21] **BOSI F. & PELLEGRINO S**, “*Molecular based temperature strain rate dependent yield criterion for anisotropic elastomeric thin film*”, Caltech, March 20, 2017
- [22] **WAKEFIELD DS & BOWN AC**, “*Non-Linear Analysis of the NASA Super Pressure Balloons : Implementation of a Large Strain Material model*”, AIAA, Pasadena, California 2015